# High Resolution Pure Rotational Spectrum of Water Vapor Enriched by H<sub>2</sub><sup>17</sup>O and H<sub>2</sub><sup>18</sup>O

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The pure rotational spectrum of a mixture of  $H_2^{16}O$ ,  $H_2^{17}O$  and  $H_2^{18}O$  between 50 and 730 cm<sup>-1</sup> was recorded on the Fourier transform spectrometer at the University of Oulu. The resolution achieved was about 0.010 cm<sup>-1</sup> and the precision of the unblended lines was better than 0.001 cm<sup>-1</sup>. About 1100 lines were assigned. The measured line positions of  $H_2^{17}O$  and  $H_2^{18}O$  were compared with the values derived from the rotation and distortion constants given in the literature.

#### **I. INTRODUCTION**

As our previous work (1) indicated, the rotational levels of  $H_2^{17}O$  and  $H_2^{18}O$ in the ground state are known quite inaccurately. In that work we observed the strongest lines of  $H_2^{17}O$  and  $H_2^{18}O$  because the sample was in natural abundance. In the literature there are only a few laboratory works (e.g., (1-5)) concerning the pure rotational infrared spectra of  $H_2^{17}O$  and  $H_2^{18}O$ , and they usually cover a narrow wavenumber region or the sample is in natural abundance.<sup>1</sup>

We felt there was a need for more extensive laboratory data on  $H_2^{17}O$  and  $H_2^{18}O$ , for example in the field of atmospheric research. There is also a certain purely theoretical interest in the accurate rotational spectra of light asymmetric-top molecules to test the centrifugal distortion theory.

Because of these facts we decided to extend our previous work by measuring the pure rotational spectrum of water vapor enriched by  $H_2^{17}O$  and  $H_2^{18}O$ .

## **II. EXPERIMENTAL DETAILS**

The interferograms of water vapor enriched by  $H_2^{17}O$  and  $H_2^{18}O$  were recorded on the Michelson-type Fourier transform spectrometer (9–12) constructed in our laboratory. The water sample was from Norsk Hydro with the following relative abundances of  $H_2^{16}O$ ,  $H_2^{17}O$ , and  $H_2^{18}O$ : 47, 24, and 29%, respectively. The whole region between 50 and 730 cm<sup>-1</sup> was recorded in three parts using beam splitters 12, 5, and 2.5  $\mu$ m in thickness. The measurement conditions are specified in Table I.

The interferograms, typically including 80 000-150 000 sampling points, were recorded out to an optical path difference of about 70 cm, which gives a truncation broadening of 0.0086 cm<sup>-1</sup>. The aperture broadening was kept smaller than 0.0080 cm<sup>-1</sup> in all cases, thus giving a theoretical resolution of about 0.0098

<sup>&</sup>lt;sup>1</sup> In addition there are works (e.g., (6-8)) concerning the vibration-rotation bands of H<sub>2</sub><sup>17</sup>O and H<sub>2</sub><sup>18</sup>O.

Range (cm <sup>-1</sup> )	Total pressure (Torr)	Thickness of beam splitter (µm)	Filters	Windows of gas cell	Absorption path length (m)
50 - 210	0.8	12	black polyethylene	polyethylene	1
210 - 400	0.5	5	black polyethylene	polyethylene	3
400 - 730	4.2	2.5	OCLI*, LI3200-9	KBr	3

TABLE I

The Measurement Conditions of the Spectra Shown in Figs. 1 and 2

\* Optical Coating Laboratory, INC

 $cm^{-1}$ . The theoretical resolution is defined as the half-width of the line due to the convolution of the truncation and aperture broadening profiles. The optical path difference was measured by a stabilized single-frequency He-Ne laser (13) partly constructed in our laboratory.

The spectra were computed by the fast Fourier transform of 16 384 points using mathematical filtering and phase correction (14) simultaneously. The interval between the adjacent spectral points computed was typically  $3 \times 10^{-3}$  cm<sup>-1</sup>. The line positions were computed directly from the spectral points produced by the fast Fourier transform by evaluating the center of gravity of the line in the three different ways described in our previous work (1). The wavenumber scale of the spectrum was calibrated using the most accurate rotational lines of H<sub>2</sub><sup>16</sup>O.

## **III. RESULTS**

The results are mainly represented in Figs. 1 and 2 and in Table II.

Figure 1 shows an overall view of the apodized spectrum recorded in three runs under the measurement conditions specified in Table I. In this spectrum the resolution is only  $0.014 \text{ cm}^{-1}$  because of apodization. The intensity scale of the spectrum was fixed so that the strongest line in each recording has 100% absorption in that scale. In Fig. 1 the line strengths are comparable with each other only within a narrow region, because no background correction has been made. The unapodized spectra with a resolution of about  $0.010 \text{ cm}^{-1}$  were used for assignment and for calculating the line positions. Figure 2 shows a part of the unapodized spectrum in the extended scale, verifying the achieved resolution of  $0.010 \text{ cm}^{-1}$  defined as the half-width of a weak absorption line.

Table II gives the observed wavenumbers of  $H_2^{16}O$ ,  $H_2^{17}O$ , and  $H_2^{18}O$  compared with the calculated ones. The calculated frequencies of the  $H_2^{16}O$  lines were derived from the rotational energy levels given by Flaud *et al.* (15) and the calculated wavenumbers of the  $H_2^{17}O$  and  $H_2^{18}O$  lines were derived from the constants given by Helminger and De Lucia (16). In order to convert megahertz into  $cm^{-1}$ , we used the value 2.997925 × 10<sup>8</sup> msec<sup>-1</sup> for the velocity of light.

The calculated relative intensities of the lines were taken from our previous

work (1) and they only give rough estimates, especially for the transitions with high J values, to help assignment. The intensity of the strongest line of  $H_2^{16}O$ ,  $H_2^{17}O$ , and  $H_2^{18}O$  at 202.686, 201.442, and 200.338 cm<sup>-1</sup>, respectively, was set equal to unity. However, the line strengths in Fig. 1 depend on the relative abundances of  $H_2^{16}O$ ,  $H_2^{17}O$ , and  $H_2^{18}O$  in the sample.

The precision of the line position (1, 12, 17) is better than  $\pm 10^{-3}$  cm<sup>-1</sup> for unblended lines with absorption between 20 and 85%. The precision of frequency is therefore lower for the lines which are blended or weak or broadened by absorption. As an example of blended lines we can give a doublet with the line numbers 100 and 101. Because of partial overlapping, the observed wavenumbers 96.2133 and 96.2262 cm<sup>-1</sup> of the doublet components are shifted towards each other as compared with the calculated wavenumbers 96.2089  $\pm$  0.0019 and 96.2316  $\pm$  0.0018 cm<sup>-1</sup>.

In Table II there are lines which are not clearly resolved in Fig. 1 because of apodization. Lower pressures than those given in Table I were also used in order to obtain the positions of the lines which are strong and very near each other.

Because of our earlier work (1), there were no difficulties in assigning all the observed lines due to  $H_2^{16}O$ . A majority of the lines of  $H_2^{17}O$  and  $H_2^{18}O$  were also successfully assigned with the help of the calculated wavenumbers and intensities listed in Table II. However, as it can be seen from this table, the coefficients of Ref. (16) fail to predict satisfactorily the line positions of the transitions where high J values are involved. Especially when both J and  $K_a$  are large, the difference between the observed and the calculated wavenumbers can be more than 1 cm<sup>-1</sup>. Despite the application of the Fraley-Rao interpolation rule (18), some lines remained unassigned until we got more reliable values for the levels with high J values. These were obtained in the usual manner by fitting the observed differences in frequencies to the Watson-type Hamiltonian. The results of Ref. (16) were used as the initial values for the parameters. It was also necessary to add some higher-order coefficients, e.g., the coefficient of the operator  $\hat{P}_{z}^{12}$ , so that we had 23 parameters in our Hamiltonian. After the first fit it was possible to assign additional transitions, which were then included in the fit. This process was repeated until practically all the lines of H<sub>2</sub><sup>17</sup>O and H<sub>2</sub><sup>18</sup>O appearing in the spectrum were successfully assigned. The greatest differences between the calculated and the observed wavenumbers after this procedure were less than 0.008 cm<sup>-1</sup> for both H<sub>2</sub><sup>17</sup>O and H<sub>2</sub><sup>18</sup>O lines.

We emphasize that the purpose of the fit at that stage of our work was only to complete the assignment of the spectrum. The work (19), where more attention will be paid to the statistical aspects, such as the weighting of the observations as well as the examination of different models, is now going on.

## IV. DISCUSSION

As Table II shows, we were able to improve considerably the precision of the line positions of  $H_2^{17}O$  and  $H_2^{18}O$  over the whole far-infrared spectral region. Further, our preliminary fits predict that the precision of the centrifugal distortion coefficients and energy levels can be increased by using our observed data. How-













ever, in this work we have concentrated on the strongest lines only, but after this it will be easy to continue the work concerning weaker lines and higher J values.

It was a pleasure to find out that the very weak  $H_2^{17}O$  and  $H_2^{18}O$  lines observed in the natural abundance of water in our previous work were successfully assigned. There is only one very weak "line," with the line number 111, which is probably misassigned.

The pure rotational spectra of  $H_2^{16}O$ ,  $H_2^{17}O$ , and  $H_2^{18}O$  are spread out in quite a wide range in the far infrared. The relative changes in the frequencies of the lines are large, thus requiring a flexible performance of the instrument. In this work we tried to maintain the performance of the interferometer nearly constant over the whole spectrum observed. There are, however, certain regions where the signal-to-noise ratio is lower than usual, such as the region below 80 cm<sup>-1</sup>



FIG. 2. Extended part of the unapodized spectrum of the mixture of  $H_2^{16}O$ ,  $H_2^{17}O$ , and  $H_2^{16}O$  at a total pressure of about 0.5 Torr. The spectrum is transformed from the same interferograms as in Fig. 1. Resolution is about  $0.010 \text{ cm}^{-1}$ . The half-width of the line 473 at 244.3429 cm<sup>-1</sup> is  $0.010 \pm 0.0005 \text{ cm}^{-1}$ .

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´(K',K´)-J*(K#,K") FHPQ OBS DIFF I LM	и(1,3)- и(0, и) 53. ции? 5×. циие -2 0.2088-01 (	асть из на сладова 53.5301 – 46 .2686-61 6 Асть 1 – исо ки сиськой са сядок – 46 .2685-61 6			2(1, 2)-1(1, 1) 55.2330 55.2353 -15 1592+00 6	2(2,1)-2(1,2) 55.4061 55.4083 -22 .671E-01 60	2(1,2)-1(0,1) 55.4538 55.4542 -4 .1598+00 67	<pre>&lt;( 1, 2) = 1( 0, 1) 55.7010 55.7039 -23 .1596+00 68</pre>	-( 0, 2)* -( 1, 2) - 51, 2000 - 51, 2001 - 25 , 1405+00 - 69 -2( 0, 3)* -2( 1, 2) -52, 3105 - 52 3056 - 10 - 1085,00 - 70	3(0,3)-2(1,2) 57.3482 57.3447 35.1486+00 71	6(3,3)-6(2,4) 57.3729 57.3703 26 114E-01 72	61 3, 3) - 6( 2, 4) 58.0296 56.0251 45 1148-01 73	6(3,3)=6(2,4) 58.7750 58.7759 -9 114E-01 74	7(3,5)-b(4,2) 53.9139 55.0133 5 493E-D3 75	7( 2, 4)+7( 2, 5) 59.0976 59.0966 10 .186E+01 76	7(3,4)-7(2,5) 59,4942 59,4875 54 ,1868-01 77	6(2,4)-6(1,5) 59.8679 59.8678 1 .147E-01 78	7(3,4)-7(2,5) 59.9470 59.9500 -120 .1865-01 79	b(2,4)-b(),5) 59.9652 59.950 62 147E-01 80	0[2,4]=6[1,5] 60.0572 60.0581 = 4.1475±01 81 6[3 3 3].6[3 3] 60.6572 60.6583 6.1475±01 81				3 ( 2, 2) - 3 ( 1, 3 ) 63.5795 63.5767 b . 7382-01 85	5( 2, 3)- 4( 3, 2) 63.4941 63.9960 -19 .116E-01 86	3(2,2)-3(1,3) 64.022/ 64.0222 6 .338E-01 87	5(2,3)+4(3,2) 64.9663 64.9876 -13 .116E-01 88 5(2,3)-4(3,2) 55.8663 55.85.8663 55.03 55.65.03	4 ( 3 1)* 4 2 2) 66 2434 66 2434 66 2430 4 2818-01 69	4(3,1) - 4(2,2) - 67.0986 - 67.0993 - 7.281E-01 - 41	8(3,5)-8(2,6) 67,1086 67,0993 93 330E-02 92	8(3,5)-8(2, b) 67,1750 67,1603 147 .330E-02 93	0(3,5)=6(2,5) 6(.2454 6).2450 -6 2308-02 94 4(2-1)-4(2-2) 64-0622 65-052 6 2450 0 2450 0	4(1,3)+3(2,2) 69.1957 69.1945 12.190E-01 95	4 ( 1. 3) - 3 ( 2. 2) 69.6485 69.6474 11 .190E-01 97	4 ( 1, 3) - 3 ( 2, 2) 70.0475 70.0465 10 190E-01 98	3(1,3)-2(0,2) 7].6406 71.6422 -16 9906-01 49	3(1,3)-2(0,2) 71.8977 71.8990 -12 .000F-01 100	3( 1, 3)-2( 0, 2) 72.1877 72.1894 -17 .990E-01 102	3( 3, 0)- 3( 2, 1) 72.3318 72.3322 -4 .798E-01 103	3(3,0)-3(2,1) 73.2626 73.2643 -17 .798E-01 104 5(1,1)-5(0,5) 74.007 74.104 7 84501 104	201 1.4.1.50 0.50 74.2024 74.2032 14.004 -1 0042E-01 105 50 1.4)+50 0.50 74.2174 74.2182 -8 .8468-01 306	5(1, 4) - 5(0, 5) 74.3140 74.3142 -2 .845E-01 107	4( 2, 3) - 4( 1, 4) 74.7918 74.7921 -3 .112E+00 108	H(3, 6)-7(4,3) 74.8787 74.8788 -1 .124E-02 109	4(2,3)-4(1,4) 75.1346 75.1355 -9 .112E+00 110	41 4, 57 - 91 5, 67 75, 8044 75, 4005 41 7, 522 E+02 11	U 2 D - 1 - 1 - 1 - 10.4000 - 10.4004 - 1244 - 1246-02 - 12 U 2 3). k 1 - k - 75 50k2 - 25 505k - 10 - 1055.00 - 11	6( 3 6) 7/ 4 2/ 7/ 7/ 7/ 7/ 2/ 2/ 2/ 2/ 2/ 2/ 2/ 2/ 2/ 2/ 2/ 2/ 2/	9(4, 5)-9(3, 6) 76.2849 76.2867 -18 .322E-02 11	9(4,5)-9(3,6) 77.3164 77.3174 -10 .322E-02	3( 3, 1)- 3( 2, 2) 77.3388 77.3368 20 293E-01	3(3,1)-3(2,2) 78.0796 78.0795 1 2936-01 116	11 10-3225.0 0 767.07 767.197 (0,11) -14 (2,1)
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wavenumber – observed wavenumber in  $10^{-4}$  cm<sup>-1</sup>; I: calculated relative intensity; the zero in front of decimal applies to all the numbers in this column. In the column MO:  $16 = H_2^{16}0$ ,  $17 = H_2^{17}0$ ,  $18 = H_2^{18}0$ , HDO = HD<sup>16</sup>0, and 010 = the rotational transition at the (010) level of  $H_2^{16}0$ . The same of the upper and lower levels in the rotational transition; FREQ: calculated wavenumber in cm<sup>-1</sup>; OBS: observed wavenumber in cm<sup>-1</sup>; DIFF: calculated Note. The meanings of the different columns are as follows: LN: line number; MO: molecule:  $J'(K'_n, K'_r) - J''(K'_n, K''_r)$ : rotational quantum numbers line number is used for the unresolved lines.

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I		.1995-02 .1995-01 .4576+00 .4576+00 .4576+00 .6308-01 .6308-01 .1992-01		.3415-01 .3215-01 .6826-02 .1146-01 .1066-01 .1056-01 .34155-01 .3666+00	001222-01 10122-01 101222-01 101222-01 101222-01 101222-02 101222-02 101222-02 101222-02 101222-02 101222-02 101222-02 10122222-02 1012222-02 1012222-02 101222	. 1395+00 - 1485+00 - 1485+00
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FREQ	159,4689 159,4689 159,87654 159,87654 160,1744 160,5560	161.8202 161.7902 165.31628 165.81648 165.85.8568 165.85688 165.85688810000000000000000000000000000000000	166.0146 166.2146 166.2146 166.2913 166.8913 169.4591 169.4591 170.3604 172.8917 172.8917	173.0837 173.1762 173.1762 174.8133 174.8133 175.2593 175.2593 175.2593 175.2593	1175- 11
(K, K, )-J*(K*,K")	((3, 1)-4(0, 4) (2, 8)-9(1, 9) (2, 8)-9(1, 9) (3, 8)-9(1, 9) (3, 6)-8(4, 9) (3, 1)-4(0, 4) (3, 1)-4(0, 4) (4, 5)	$ \begin{bmatrix} 3 & 5 \\ 3 & 5 \end{bmatrix} - 8 \begin{bmatrix} 4 & 5 \\ 4 & 5 \end{bmatrix} $ $ \begin{bmatrix} 3 & 5 \\ 3 & 5 \end{bmatrix} - 4 \begin{bmatrix} 0 & 4 \\ 4 & 5 \end{bmatrix} $ $ \begin{bmatrix} 3 & 5 \\ 2 & 5 \end{bmatrix} - 5 \begin{bmatrix} 7 & 2 \\ 1 & 5 \end{bmatrix} $ $ \begin{bmatrix} 2 & 5 \\ 2 & 5 \end{bmatrix} - 5 \begin{bmatrix} 7 & 1 \\ 1 & 1 \end{bmatrix} $			
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	7)- 8( 2, 5) 232.0442 232.05 3)-10( 1, 9) 232.1179 232.11	رد ۱۰ - د	223 .176E -1 .803E	103	114	) 7	m <del>-</del>			6 ( 4 7	263.2695	262.8389	- 150	.365E-03 .666E-03
710         -770         54.377         54.377         54.3797         54.377         54.3797         54.377         54.3797         56.3767         55.44.377         56.3767         55.44.377         56.3767         55.44.377         56.44.376         56.4.376         56.4.37	8)-10(4,7) 233.1454 232.979 7)-8(2,6) 233.3200 233.320		57 .233E 0 .176E	-01 5	11 11	12(	a. w 4 0	8) 6 2)11		6 e e	263.2872 263.7953	263.2845 263.5165	27 2788	.773E-01 .765E-03
1000         1000 <th< td=""><td>8)-10(4,7) 233.9213 233.913 2)-13(0,13) 234.7420 234.700</td><th>2</th><td>81 .233E</td><td>103</td><td>117 118</td><td>12(</td><td>3, 9</td><td>===</td><td>÷.</td><td>66</td><td>264.0834</td><td>264.0754</td><td>80</td><td>.365E-D3</td></th<>	8)-10(4,7) 233.9213 233.913 2)-13(0,13) 234.7420 234.700	2	81 .233E	103	117 118	12(	3, 9	===	÷.	66	264.0834	264.0754	80	.365E-D3
	2)-13( 0,13) 235,6109 235,200		04 505E	5	118 17	100	40	- e		1	264.6508	264.6550	24	.7738-01
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111         211 <td>8)- 9( 2, 7) 242.0860 242.0688 ?)- 3( 0, 3) 242.9555 242.9552</td> <th>•</th> <td>-28 .243E 3 .406E</td> <td>-01</td> <td>21 18</td> <td> </td> <td> </td> <td></td> <td>-0</td> <td>22 22</td> <td>265.7687</td> <td>265.7079</td> <td>608 626</td> <td>.140E-02</td>	8)- 9( 2, 7) 242.0860 242.0688 ?)- 3( 0, 3) 242.9555 242.9552	•	-28 .243E 3 .406E	-01	21 18	 	 		-0	22 22	265.7687	265.7079	608 626	.140E-02
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9.2       0.005-01       527       10       111       266.9973       266.9973       266.9475       267.9460       276.9416       276.9425	8)-9(2,7) 244.2070 244.2073		-3 .243E	101	11	1				Ê	266.3959	266.2416	1543	.4208-02
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	3) - 5( 2, 4) 244, 4422 244, 4428		-6 .1052	s 00+	26 16	Ĩ	1			ŝ	266.8446	266.8452	- 6	.1405-02
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5. 1056-00         55 10         57.540         57.550         57.540         57.550         57.540         57.550         57.550         57.550         57.550         57.550         57.550         57.550         57.550         57.550         57.550         57.550         57.550         57.550         57.550         57.550         57.550         57.750         77.912         77.112         77.711         77.7	3)- 5( 3, 2) 245.3056 245.3063		-7 . 1040E	5 000+	28 18	ñ æ		8 - (1		29	266.9909	266.9841	5095 68	.3786-02 .4316-03
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17.1         17.1 <th17.1< th="">         17.1         17.1         <th1< td=""><td>3) - 5(3, 2) - 246.5330 - 246.5311</td><th>. '</th><td>3011. 01</td><td>00+</td><td>31 16</td><td>i E</td><td>2,12</td><td>-15</td><td>ŝ-</td><td>22</td><td>267.7554</td><td>267.7585</td><td></td><td>.3786-02 .1266-02</td></th1<></th17.1<>	3) - 5(3, 2) - 246.5330 - 246.5311	. '	3011. 01	00+	31 16	i E	2,12	-15	ŝ-	22	267.7554	267.7585		.3786-02 .1266-02
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1033     31056-02     535     18     95     410     1134     700     710     195     61       1031     11056-00     537     17     15     700     193     193     193       282     3006-00     537     17     125     3100-111     2     9     771     193     1936     1936       282     31056-02     539     100     75     10     10     10     193     1936       283     3105     100     75     10     11     20     210     210     210       284     3105     100     75     10     10     27     114     20     1336       284     3105     100     75     10     10     27     210     193       283     1114     10     27     210     27     211     210     210       283     119     10     27     210     27     211     210     210       284     1016     27     10     27     217     211     210     211       284     1016     100     27     210     210     210     210     210       284     1016     27	3)-12( 1,12) 247.7926 247.7633	. Á	3411 . 56	5.0	34 18	12(			v v v	6	2200.1987	270.2146	- 159	-431E-03
110         -1115         -112 <td< td=""><td>3)-12( 0,12) 247.7966 247.7633</td><th>m</th><td>3086. 55</td><td>-02 5</td><td>35 18</td><td>6</td><td>5</td><td>6 - (</td><td>2</td><td>:5</td><td>270.4247</td><td>270.4121</td><td>126</td><td>.8178-03</td></td<>	3)-12( 0,12) 247.7966 247.7633	m	3086. 55	-02 5	35 18	6	5	6 - (	2	:5	270.4247	270.4121	126	.8178-03
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28         3002-00         539         HD0         7         1         7         9640         7         9640         7         9640         7         9640         7         9640         7         9640         7         9640         7         9640         7         9640         7         9640         7         9640         7         9640         7         9640         7         9640         7         9640         7         9640         7         9640         7         9640         7         9640         <	3)-12( 1, 12) 248.3473 248.2633	æ	40 .1146	- 01	38 16	12(	3, 10		~	6	271.8427	271.8431	- <del>-</del>	. 397E-02
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4.5       1.5       3.1       6.5       3.1       3.1       3.1       3.1       3.1       3.1       3.1       3.1       3.1       3.1       3.1       3.1       3.1       3.1       3	1)+11( 1, 10) 248.7955 246.7978	i	-23 101E	10	11 04	6	5	5		12	272.7129	272.7219	-90	.817E-03
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T. T. T. T. C.	))- 4( 4, 1) 253.9685 253.9641 ().14( 1 14) 254 2054 258 2080		44 .701E	400 400	56 16	98	~ " • •		Ĵ	ີ	278.5184	278.5181	~ .	.1458+00
7         402E-02         559         18         5(1, 5)         279.3300         279.3325         -25         1458E-03           1         46         402E-02         560         18         5(1, 5)         21.4(0, 4)         279.3365         79.356         3         2002E-01           1         9         46         402E-02         560         18         5(1, 5)         34         260.3166         2         2392+01           2         3         1         344         30.4(1, 4)         34         260.3166         2         2392+01           3         3         1         3482         290.3166         2302.3186         2         2792+01         2         2392+00           3         3         13442         260.3166         3(4, 5)-7(1, 6)         2         2804435         802.4435         <	1)-10( 2, 8) 255.2504 255.258		77 , 3446	-05	58 18		n ⊷ • 10			ì	278.8807	278.8764	109	.1062+00
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I	0.144E-03 .191E-02 .334E+00	.432E-03	.3936-03 .1326-03 #336-03	.4328-03	.1428-02	E0-3664.	.499E-03	.187E-02	.142E-02	.187E-02	.1875-02	.3656-01	.365E-01 64EE-02	.3658-01	.185E-03	.3895-04	.1246-03	.1085-03	.1115+00	.586E-01 .160E-03	.586E-01	.111E+00	.181E+00	.6028-01	.1305-03	.370E-01	.181E+00	.1598-03	.3706-01	.740E-03	.1518-03	. 562E-02	.6628-02	.572E-01
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FREQ	302.8156 302.8021 302.9817 302.9817	303.1106	303.3577 303.3904 304.4713	304.5988	305.6887	306.2695	306.4179 307.4646	308.1935	309.4723	309.81418	311.7291	313.6798	314.3458	315.0820	320.4131	320.4134	320.791	321.1244	322.1937	322.4081	323.6310	323.9595	324.1015	325.7042	325.8644	326.6540	327.5948	327.8230	328.1683	329.6287	331.2991	332.0324	334.6168	335.1303 335.1575
J ( K , K ) - J = ( K , K ) ) J ( K , K )	14(2,12)-13(3,11) 11(4,8)-10(3,7) 6(6,1)-5(5,0) 6(6,0)-5(5,1)	14(3,12)-13(2,11) 7(5,2)-6(4,3)	15( 2, 14)-14( 2, 13) 15( 2, 14)-14( 1, 13) 14( 3, 12)-13( 2, 11)	14(3,12)-13(2,11)		8(3,5)-8(0,8)	8(3,5)-8(0,8) 6(4,3)-6(1,6)	12(4,9)+11(3,8) 11(5,6)-11(2,9)	6(4,3)-6(1,6)	12( 4, 9)-11( 3, 8)	12(4,9)-11(3,8)	B( 4, 4) - 7( 3, 5)		8(4,4)-7(3,5)	17( 0, 17)-16( 1, 16)	17( 1, 17)-16( 0, 16) 8( 5, 4)-7( 4, 3)	15( 2,13)-14( 3,12)	16( 2,15)-15( 1,14)	8(5, 4)-7(4, 3)	6(3,4)-5(0,5) 10(4,6)-10(1,9)	6(3,4)-5(0,5)	7( 6, 2)- 6( 5, 1)	7( 0, 1)- 6( 5, 2) 8( 5, 3)- 7( 4, 4)	7( 6, 2)- 6( 5, 1)	5(5,1)-5(2,4)	B(5,3)-7(4,4) 7(5,2)-6(5,1)	7( 6, 1)- 6( 5, 2)	6 ( 6, 0)- 5 ( 5, 1)	8(5,3)-7(4,4)	6( 5, 2)- 6( 2, 5) 5( 4, 2)- 4( 1, 3)	14(4,11)-13(3,10)	5(4,2)-4(1,3) 6(5,2)-6(2,5)	5(4,2)-4(1,3)	7(2,5)-6(1,6)
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J'(K', K')-J"(K", K") a	9(4,5)-9(1,8) 280.7 9(4,5)-9(1,8) 281.1 7(4,3)-6(3,4) 281.2 5(4,3)-6(3,4) 281.2	5(3, 3) - 4(0, 4) 281.91 6(5, 1) - 6(2, 4) 282.16	7(4,3)-6(3,4) 282.25 13(2,11)-12(3,10) 283 34 5(7,3)-5(15) 283 348		13( 2,11)-12( 3,10) 284.23	15( 1,15)-14( 0,14) 284.39	14(1,13)-13(2,12) 284,30 13(2,11)-12(3,10) 284,37	14( 2,13)-13( 1,12) 284.38 15( 0,15)-14( 1,14) 284 74		14( 2,13)-13( 1,12) 285.49	14(1,13)-13(2,12) 285.51	6( 2, 1) = 6( 2, 4) 285,85	13( 3,11)-12( 2,10) 286.32	13(3,11)-12(2,10) 287,38	9(4, 6)- 8(3, 5) 287,15 13(3,11)-12(2,10) 287,859	5(5,0)-5(2,3) 288.52		7(3,4)-6(2,5) 289,44	13( 3, 10)-12( 4, 9) 289.77 13( 3, 10)-12( 4, 9) 290.48	13(3,10)-12(4,9) 290.20 9(4,6)-8(3,5) 290.72	5(5,0)-5(2,3) 291.82	10(4,1)-9(3,6) 294.6 .5(5,0)-5(2,3) 295.56	10(4,7)-9(3,6) 296.3 10(4,7)-9(3,6) 298.4	7(5,3)-6(4,2) 298.80	6(6, 0)-5(5, 1) 299.51	7(5,2)-6(4,3) 300.17 7(5,3)-6(4,2) 300.24	7(4,3)-6(3,4) 300.43	11(4,8)-10(3,7) 301.11	6( 6, 1)-5( 5, 0) 301.1	0( 0, 0)- 5( 5, 1) 301.1 <sup>4</sup> 16( 0,16)-15( 1,15) 301.5	16( 1, 16)-15( 0, 15) 301.55	7(5,21-6(4,3) 301.6 7(5,3)-6(4,2) 301.8	16(0,16)-15(1,15) 302.3	16( 1,16)-15( 1,15) 302. 16( 1,16)-15( 0,15) 302.
۳۵ J'(۲',۲') مار مار ۲',۲') مار مار ۲',۲') مار ۲',۲')	17 9(4,5)-9(1,8) 280.7 16 9(4,5)-9(1,8) 281.1 17 1(4,5)-5(1,5) 281.2 17 6(4,2)-6(1,5) 281.2	16 5( 3, 3) - 4( 0, 4) 282.19 17 6( 5, 1) - 6( 2, 4) 282.16	16 7(4,3) - 6(3,4) 282.25 18 13(2,11) - 12(3,10) 283.34 16 5(7,2) - 5(1,5) 283.34		17 13( 2,11)-12( 3,12) 284.23	17 15( 1,15)-14( 0,14) 284.39	18 14(1,13)-13(2,12) 284,30 16 13(2,11)-12(3,10) 284,37	18 14(2,13)-13(1,12) 284.38 16 15(0,15)-14(1,14) 284.78		17 14(2,13)-13(1,12) 285.49	16 14( 1,13)-13( 2,12) 285,51 • • • • • • • • • • • • • • • • • • •	16 6(5, 1) = 6(2, 4) 285,05	16 13(3,11)-12(2,10) 286.32	17 13( 3, 11)-12( 2, 10) 287, 38	16  9(4, 5) - 8(3, 5)  287, 15 16  13(3, 11) - 12(2, 10)  287, 85	18 5(5,0)-5(2,3) 288.52 17 0(1,5) 6(2,5) 288.52			15 13( 3,10)-12( 4, 9) 289.77 17 13( 3,10)-12( 4, 9) 290.48	18 13(3,10)-12(4,9) 290.20 16 9(4,6)-8(3,5) 290.72	17 5(5,0)-5(2,3) 291.82	10 10( 4, 7)- 9( 3, b) 294.5 16 . 5( 5, 0)- 5( 2, 3) 295.56	17 10(4,7)-9(3,6) 296.3 16 10(4,7)-9(3,6) 294.4	18 7(5,3)-6(4,2) 298.80	18 6( 6, 0)-5( 5, 1) 299.51	18 7(5,2)-6(4,3) 300.17 17 7(5,3)-6(4,2) 300.24		18 11(4, 8)-10(3, 7) 301.11	17 6( 6, 1)- 5( 5, 0) 301.1	17 0( 0, 0)- 5( 5, 1) 301.1 <sup>4</sup> 18 10( 0,10)-15( 1,15) 301.5	18 16( 1,16)-15( 0,15) 301.55	17 7(5,21-6(4,3) 301.5 16 7(5,3)-6(4,2) 301.8	17 16(0,16)-15(1,15) 302.3	16 16( 0,16)-15( 1,15) 302. 16 16( 1,16)-15( 0,15) 302.

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۲`(لاً لارٌ)، استرلام، لام") FREQ OBS DIFF I	12(4,9)-11(1,10) 598.9822 598.9991 -169 0.984£-03 11(6,6)-10(3,7) 599.4605 599.7031 -246.01344£-03 121.6,6)-10(3,7) 500.1035 500.1036 -10	11( 6, 6)-10( 3, 7) 604,4471 604,4489 -18 176E-03	7(5,3)-6(0,6) 606,1492 606,1459 33 .871E-04 7(5,3)-6(0,6) 609,3449 609,3370 79 .871E-04	12(6,7)-11(3,8) 612.6499 612.5227 1272 2185-03 71 5 3)-61 0 5) 612.9502 612.9510 -8 8715-05	9( 4, 5)- 8( 1, 8) 614.2077 614.2003 74 .843E-03	9(4,5)-8(1,8) 615.0890 615.0649 241 .843E+03 of 4.5)-8(1,8) 616.0728 616.0720 8 843E+03	12( 6, 7)-11( 3, 8) 615.9058 616.2795 -3737 .218E-0	9( 6, 3)- 8( 3, 6) 617.3709 617.3506 203 .787E-03	9( 6, 3)- 8( 3, 6) 621.0526 621.0616 -90 .787E-02	13( 5, 9)-12( 2,10) 623.4389 623.2931 1458 .609E-0	13(5,9)=12(2,10) 624.5685 624.7031 -1345 .6098=04 64.6.31_84.3.61.625.2684 625.2675 6 .7878=05	13(5, 9)-12(2,10) 626.3206 626.3221 -15 .609E-0	7(7,1)+6(4,2) 626.8000 626.7990 10 .6528-0	1 1 1 01- 01 4, 31 021.4540 021.52359 1 1 1098-0. 151 2 101_111 1 11 621 1758 631.2178 -420 .3056-0	7(7,1).6(4,2) 631.5997 631.6079 -82 .652E-0	12( 2,10)-11( 1,11) 632.3225 632.1073 2156 .305E-0	7(7,0)-6(4,3) 632.7085 632.7145 -60 .109E-0 .0/2.0111/11/21220988 532.0402 8 2055-0	12( 2,10)-11( 1,11) 033,0000 033,0092	12( 3,10)-11( 0,11) 634.4256 634.2366 1890 .9168-0	12[ 3,10)-11( 0,11) 635.3945 635.3973 12 .916E-0	7( / 1) = 0( 4, 2) 03(+035) 03(+035) 2 +0345=0 7( 7 0) = 6( 1 3) 638 0601 638 0000 +0 1866=0	13(3,10)-12(2,11) 639.4356 639.4325 31 .286E-0	13(3,10)-12(2,11) 639.9864 639.7045 2819 .286E-0	13(3,10)-12(2,11) b39.9736 b39.9723 13 .200E-U	10(5,5)-9(2,0) 040,5101 040,5403 190 -2355- 10(5,5)_0(2,3) 640,1535 640,1635 -100 -2335-(	10(5,5)-9(2,8) 644,3218 644,3201 17 ,233E-0	8(7, 2)-7(4, 3) 648.9809 648.9785 24 .347E-0	13( 4,10)-12( 1,11) 649.5527 649.5580 -53 .106E-C	13( 4,10)-12( 1,11) 050.6157 050.6157 050.4,101 101-120 131 4,10)-121 111, 651.5758 651.5804 -46 1065-0	10(6, 4)-9(3, 7) 651.8754 651.8346 408 .143E-0	8(7, 1)-7(4, 4) 652.7857 652.7842 15 .104E-0	8(7,2)-7(4,3) 653,8954 653,901256 34716-0 10(6,1)-9(3,7) 555,2340 655,2969629 ,14315-0	8(7, 1)-7(4, 4) 657.5583 657.5568 15 .104E-C	10( 6, 4)- 9( 3, 7) 659.2320 659.2316 4 .1438-0 Ar 7 2)- 7/ 4 2) 650 4530 659.2530 0 3478-0	8( 5, 4)-7( 0, 7) 662.5973 662.5913 60 .207E-(	8(7,1)-7(4,4) 662.9465 552.9485 -20 .104E-C 81 5 B)-7(0,7) 555 5550 555.5483 -24 .2017E-C	0 ( 7, 3) - 8 ( 4, 4) 667.9576 667.9365 211 .127E-0	8(5, 4)-7(0,7) 668.9236 668.9230 6 .207E-0	14(5,10)+13(2,11) 671.3560 671.3636 -76 492E-0	9(7,3)=8(4,4) 072.9960 073.04/7 -511 .12/12=1 of 7 3).8/1 2 57 7557 577.7120 227 28212-0	g(7, 3)- 8(4, 4) 678.8078 678.8074 4 .127E-	9(7, 2)+ 8(4, 5) 682.4751 682.5027 -276 .282E-	10( 7, 4)- 9( 4, 5) 082.7959 082.1342 014 .34345 13( 2.11)-12( 1.12) 686.7383 686.8269 -886 .984E-	13(3,11)-12(0,12) 687.7420 687.8287 -867 0.1038-	
НО J'(K <sup>*</sup> , K <sup>*</sup> ) + J'*(K <sup>*</sup> , K <sup>*</sup> ) FREQ OBS DIFF I	17 12(4,9)-11(1,10) 598.9822 598.9991 -169 0.984E-03 17 11(6,6)-10(3,7) 599.465 599.7031 -242 176E-03 14 103.6.01-110(3,7) 500.1035 500.1034 -1 544E-03	10 11( 0, 0)-10( 3, 7) 604,4471 604,4489 -18 .176E-03	18 7(5,3)-6(0,6) 606,1492 606,1459 33 .871E-04 17 7(5,3)-6(0,6) 609,3449 609,3370 79 .871E-04	18 12(6,7)-11(3,8) 612.6499 612.5227 1272 2185-03 16 71 6 31-61 0 6) 612.9502 612.9510 -8 8715-04	18 9( 4, 5)- 8( 1, 8) 614.2077 614.2003 74 .843E-03	17 9(4,5)-8(1,8) 615.0890 615.0649 241 .843E+03 16 of u.c)-8(1,8) 616.0728 616.0720 8 .843E+03	17 12(6, 7)-11(3, 8) 615.9058 616.2795 -3737 .218E-0	18 9( 6, 3)- 8( 3, 6) 617.3709 617.3506 203 .787E-03	17 9( 6, 3) - 8( 3, 6) 621.0526 621.0616 -90 .787E-0	18 13( 5, 9)-12( 2,10) 623.4389 623.2931 1458 ,609E-0	17 13(5,9)=12(2,10) 624.5685 624.7031 -1340 .6098=04 16 04 6 31 84 3 61 625 2681 625 2675 675	16 13(5, 9)-12(2,10) 626.3206 626.3221 -15 .609E-0	16 7( 7, 1)- 6( 4, 2) 626.8000 626.7990 10 .6528-0	10 // / // // // // // // /// //////////	17 7( 7, 1), 6( 4, 2) 631,5997 631,6079 -82 ,6528-0	17 12( 2,10)-11( 1,11) 632.3225 632.1073 2156 .305E-0	17 7(7,0)-6(4,3) 632.7085 632.7145 -60 .109E-0	10 12( 2,10)-11( 1,11) 000,000 000,000 20,000 20 20 2002-00 20 20 20 20 20 20 20 20 20 20 20 20 2	17 12( 3,10)-11( 0,11) 534.4256 534.2365 1890 .916E-0	16 12[ 3,10)-11( 0,11) 635.3985 535.3973 12 .916E-0	10 7( 7, 1)- 0( 4, 2) 03(-033) 03(-033) 2 -0326-0 ++ 7: 7 0). 4: 1 3) 638.0801 638.0000 -4 -1896.0	18 13 3.10)-12( 2.11) 639.4356 639.4325 31 .286E-0	17 13(3,10)-12(2,11) 639.9864 639.7045 2819 .286E-0	16 13(3,10)-12(2,11) b39.9736 b39.9723 13 .2005-0 .0 .07 5 5) 57 5 51 510 3101 510 3002 108 3335-0	10 10 10 5. 5. 9. 5. 0. 040.510 10.520.5 10 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5.	16 10(5,5)+9(2,8) 644.3218 644.3201 17 2335-0	18 8(7, 2)-7(4, 3) 648.9809 648.9785 24 .347E-(	18 13(4,10)-12(1,11) 649.5527 649.5580 -53 .106E-C	17 13(4,10)-12(1,11) 050.0157 050.010 1020 . 	18 10( 6, 4)- 9( 3, 7) 651.8754 651.8346 408 .143E-0	18 8(7,1)-7(4,4) 652.7857 652.7842 15 .104E-0	17 B( 7, 2)+ 7( 4, 3) 653,8954 653,9012>6 ,347E+0 17 10( 6, 4)- 9( 3, 7) 255,2340 655,2969629 ,143E+0	17 8(7, 1)-7(4, 4) 657.5583 657.5568 15 .1048-0	16 10(6,4)=9(3,7) 559.2320 559.2315 4 .143E-0 16 Ar 7 2)_7(4 2) 650 4530 659.4530 0 347E-0	18 8(5, 4)-7(0, 7) 662.5973 662.5913 60 .207E-(	16 B( 7, 1)-7( 4, 4) 662.9466 662.9486 -20 .104E-C 17 B( F H)-7( 0 -7) 665 5550 666.5583 -201 .2075-C	18 0(7,3)=8(4,4) 667.9576 667.9365 211 127E-0	16 8(5, 4)-7(0, 7) 668.9236 668.9230 6 .207E-0	16 14(5,10)-13(2,11) 671.3560 671.3636 -76 492E-0	17 9(7,3)=8(4,4) 672,9966 673,0477 =511 ,1275=0 18 6(7,3)=8(4,4) 672,7567 677,7440 -227 ,2828=0	16 9(7, 3)- 8(4, 4) 678.8078 678.8074 4 .127E-	17 9( 7, 2)+ 8( 4, 5) 682.4751 682.5027 -276 .282E-	18 10( 7, 4)- 9( 4, 5) 082.7959 082.1345 014 .323557 18 13( 2.11)-12( 1.12) 686.7383 686.8269 -886 .98455	18 13( 3,11)-12( 0,12) 687.7420 687.8287 -867 0.103E-	

and that around  $400 \text{ cm}^{-1}$ . The transmission of the interferometer was low in these regions. This disadvantage could be cancelled by using more than three different thicknesses of the beam splitter.

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